# Study of Gd-Y Alloys for Use in Cycle of Active Magnetic Regeneration

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## **ABSTRACT**

Until now, gadolinium (Gd) has been used as a magnetic refrigerant in room temperature magnetic refrigeration studies based on the Active Magnetic Regeneration (AMR) cycle. However, with this material, the working temperature region is restricted by the value of magnetic entropy change ( $\Delta S_{\rm m}$ ), which shows a sharp peak near the Curie temperature ( $T_{\rm c}$ ). In order to expand the working temperature region of Gd, it may be possible to use layered structures of magnetic refrigerants with different  $T_{\rm c}$  so as to achieve a broader region of magnetic entropy change.

In this study, we analyzed the  $T_{\rm C}$  and  $\Delta S_{\rm m}$  of Gd-Y alloys to identify suitable magnetic refrigerants for use in a layered structure. Details are presented which show that the  $T_{\rm C}$  of Gd-Y alloys is easily controllable, and that the refrigerating capacity of Gd-Y alloys is almost equivalent to that of Gd.

# INTRODUCTION

In recent years, magnetic refrigeration based on the magnetocaloric effect has attracted attention as a candidate technology for minimizing impact to the Earth environment and minimizing global warming. A key advantage of magnetic refrigeration is that it does not use chlorofluorocarbons that can negatively influence ozone layer depletion.

Operation near room temperature places new demands on magnetic refrigeration that may be fulfilled by the AMR cycle, as this cycle is expected to be able to expand the working temperature region from low temperature to room temperature. Over the past few years there have been many studies of magnetic refrigeration using superconducting magnets or permanent magnets in the AMR cycle in the room temperature region.<sup>1-7</sup>

In these studies, ferromagnetic materials, such as Gd, have been used as the magnetic refrigerant. The value of  $\Delta S_{\rm m}$  of ferromagnetic materials shows a peak near  $T_{\rm C}$ , and the  $\Delta S_{\rm m}$  decreases as the temperature separates away from the  $T_{\rm C}$  temperature. This is one of the reasons that the working temperature region of the AMR cycle with ferromagnetic materials has been restricted. In order to apply room-temperature magnetic refrigeration techniques to practical use, the working temperature region must be greater than 30 K. One possible means of expanding the working temperature region of Gd, is to use layered structures of magnetic refrigerants with different  $T_{\rm C}$ .

The purpose of this study was to investigate the magnetocaloric effects and the working temperature region of Gd-Y alloys as possible candidates for use in layered-structure magnetic refrigerants.

## **EXPERIMENTAL METHOD**

Gd and Y of 99.9 % purity were used for the production of the Gd-Y alloys. The composition ratios of Gd-Y alloy samples, as a ratio of atoms, were Gd98-Y2, Gd96-Y4, Gd94-Y6, Gd92-Y8 and Gd90-Y10. After weighing the bits of metal of Gd and Y, they were melted using arc-melting equipment. In order to increase the homogeneity of the alloys, the melting was performed four times. After the melting, we achieved alloys in the shape of a button about 3 cm in diameter.

To accurately perform the magnetization measurements it was necessary to make the alloys the shape of a slender rod so that a demagnetizing field would not influence the alloys. The alloys of the shape of a button were cut into the shape of a rod with an aspect ratio of 1:8. The mass of the rod-like samples was about 4.5 mg. The temperature dependence and magnetic field dependence of magnetization of these rodlike samples were measured using a Superconducting Quantum Interference Device (SQUID) magnetometer.

## RESULTS AND DISCUSSION

Y content (at %)

Figure 1 shows the temperature dependence of magnetization of the Gd and Gd-Y alloys. The Curie temperature  $T_C$  corresponds to the inflection point of magnetization. Each magnetization is normalized with the value at 150 K so that  $T_{\rm C}$  may become intelligible. The  $T_{\rm C}$  of Gd90-Y10 is estimated to be 273 K from the graph, while the  $T_C$  of Gd is 294 K, as is generally known. In the range from 273 K to 294 K, it turns out that  $T_{\rm C}$  gradually moves to lower temperatures as the Y content increases. The  $T_{\rm C}$  of all Gd-Y alloys were estimated from Figure 1 and are listed in Table 1.

Referring to Table 1, Figure 2 shows the Y content dependence of the  $T_c$  of Gd-Y alloys. Depending on the Y content, the  $T_{\rm C}$  drops in temperature almost linearly: for each 1 at% of Y that is compounded, the  $T_C$  falls 2 K.

Next, we discuss the value of  $\Delta S_{\rm m}$  of Gd and Gd-Y alloys. The value of  $\Delta S_{\rm m}$  of ferromagnetic

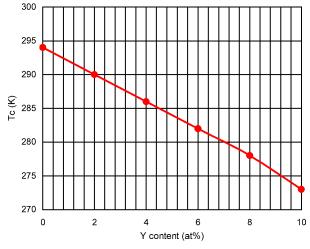
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273

<i>T</i> <sub>C</sub> (K)	294	290	286	282	278
1.2					
			-	Gd100 -	Gd98-Y2
1	,			Gd96-Y4 =	<del>×</del> Gd94-Y6
' <u>T</u>				Gd92-Y8 -	Gd90-Y10
Magnetization (a.u.)		-			
io l					
0.6 siz					
gnet			'		
ğ 0.4 -				<del>-                                      </del>	
0.2				<del>-        </del>   -	<b>\</b>
				1/4/1	.\
ا ه				-	
15	0 180	210	240		300 330
Temperature (K)					

**Table 1.** The Curie temperature of Gd-Y alloys.

Figure 1. Temperature dependence of magnetization of Gd-Y alloys; each magnetization curve is normalized to unity at 150 K.



**Figure 2.** Dependence of  $T_c$  on Y content in Gd-Y alloys.

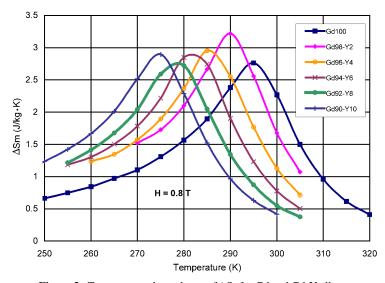
substances can be derived using Maxwell's relation. Maxwell's relation is shown below as Equation (1).

$$\left(\frac{\partial S(T,H)}{\partial H}\right)_{T} = \left(\frac{\partial M(T,H)}{\partial T}\right)_{H} \tag{1}$$

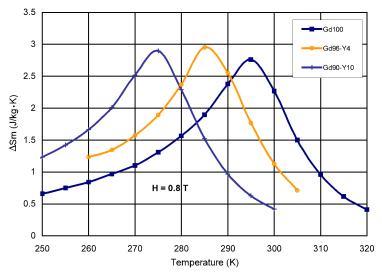
$$\Delta S_{M}(T,H) = \int_{0}^{\Delta H} \left(\frac{\partial M(T,H)}{\partial T}\right)_{H} dH$$
 (2)

The value of  $\Delta S_{\rm m}(T,\Delta H)$  of Gd and Gd-Y alloys can be estimated from Equation (2) using magnetization measurement results and the temperature dependence and magnetic field dependence of the magnetization.

Figure 3 shows the temperature dependence of  $\Delta S_{\rm m}$  of Gd and Gd-Y alloys with changing magnetic field strength from 0 to 0.8 T ( $\Delta H$ =0.8 T). The peak value of  $\Delta S_{\rm m}$  of Gd with  $\Delta H$ =0.8 T is about 2.8J/kg·K. The magnetic field strength of 0.8 T can be obtained with ordinary permanent



**Figure 3.** Temperature dependence of  $\Delta S_m$  for Gd and Gd-Y alloys.



**Figure 4.** Temperature dependence of  $\Delta S_m$  for Gd and Gd-Y alloys.

magnets. The value of  $\Delta S_{\rm m}$  of each Gd-Y alloy achieves a peak around the  $T_{\rm C}$ , and the peak temperature shifts to the lower temperature side gradually. It is also observed that the peak values of  $\Delta S_{\rm m}$  of the Gd-Y alloys are almost equivalent to that of Gd.

## **CONCLUSIONS**

We have confirmed that the  $T_{\rm C}$  of Gd-Y alloys is easily controllable in the range from 273 K to 294 K; in fact, the  $T_{\rm C}$  of Gd-Y alloys drops in temperature almost linearly with the Y content. We also have determined that the refrigerating capacity of Gd-Y alloys is almost equivalent to that of Gd, because the peak value of  $\Delta S_{\rm m}$  of Gd-Y alloys and that of Gd are practically equal. Thus, we conclude that Gd-Y alloys will be suitable for use in layered structures of magnetic refrigerants.

Figure 4 shows the temperature dependence of  $\Delta S_{\rm m}$  of Gd100, Gd96-Y4 and Gd90-Y10. This is representative of a 3-layered-structure magnetic refrigerant where the working temperature region or each of the three components has been shifted by 10 K. Such a magnetic refrigerant has the potential of maintaining a high value of  $\Delta S_{\rm m}$  over the indicated temperature region. In the future, we will investigate the appropriate interval of the working temperature region.

Figure 5 shows the spherical particles of the Gd-Y alloy; the diameter is about 1 mm. We will try and use the Gd-Y spherical particles for a layered structure.

## **ACKNOWLEDGMENTS**

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Figure 5. Spherical particles of Gd-Y alloy.

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